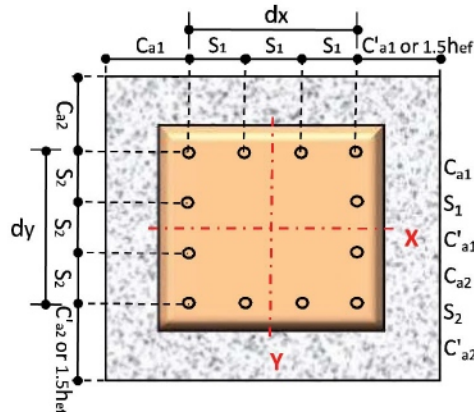


DESIGN OF ANCHOR SYSTEM IN CONCRETE

ACI 318M-11 APPENDIX D

1. Input Data:

Type of Anchor	Cast-In Anchors	No. of Intermediate Anchors along X-Direction(one side), n_x	$n_x = 0$
Grade of Anchor	8.8	No. of Intermediate Anchors along Y-Direction(one side), n_y	$n_y = 0$
Anchor Diameter, d_a	= 24 mm		
Compressive Strength of Concrete, f'_c	= 32 MPa		
Anchor Embedment Depth, h_{ef}	= 600 mm		



C_{a1}	=	120	mm
S_1	=	210	mm
C'_{a1}	=	120	mm
C_{a2}	=	120	mm
S_2	=	210	mm
C'_{a2}	=	120	mm

Total No. of Anchors: $N = 4$

Total No. of Anchors along X-Direction(one side) = 2

Total No. of Anchors along Y-Direction(one side) = 2

2. Applied Loads

Ultimate Tension, N_U	=	0	kN
Ultimate Moment along X-direction, M_{UX}	=	25	kN.m
Ultimate Moment along Y-direction, M_{UY}	=	0	kN.m
Ultimate Shear along X-direction, V_X	=	0	kN
Ultimate Shear along Y-direction, V_Y	=	4	kN

3. Verification of Anchors against Tension Clause D.5

For Single Anchor:

Check Applied Tension for each Anchor, N_{ua}

Tension on each Anchor due to N_U , T_A	=	N_U/N	=	0.00	kN
Tension on each Anchor due to M_{UX} , T_X	=	$(M_{UX}/dy)/N_x$	where: N_x	=	No. of anchors for M_{UX}
	=	59.524	kN	=	2
Tension on each Anchor due to M_{UY} , T_Y	=	$(M_{UY}/dx)/N_y$	where: N_y	=	No. of anchors for M_{UY}
	=	0.00	kN	=	2

$$N_{ua} = T_A + T_X + T_Y = 59.524 \text{ kN}$$

For Anchor Group:

Check Applied Tension for group of anchors, N_{uag}

Tension due to N_U , T_G	=	N_U	=	0	kN
Tension due to M_{UX} , T_{GX}	=	(M_{UX}/dy)	=	119.05	kN
Tension due to M_{UY} , T_{GY}	=	(M_{UY}/dx)	=	0	kN

$$N_{uag} = T_G + T_{GX} + T_{GY} = 119.05 \text{ kN}$$

DESIGN OF ANCHOR SYSTEM IN CONCRETE

ACI 318M-11 APPENDIX D

3.1. Steel Strength of Anchors

Clause D.5.1

Tension Capacity of each Anchor, ϕN_{sa} :

$$\phi N_{sa} = \phi A_{se,N} f_{uta}$$

where:

$$\phi = 0.7 \quad \text{Clause D.4.3}$$

$$A_{se,N} = \text{Effective Cross-Sectional Area of Anchor} = 245.04 \text{ mm}^2$$

$$f_{uta} = \text{Nominal Tensile Strength of Anchors} = 800 \text{ MPa}$$

$$N_{sa} = 196.0 \text{ kN}$$

$$\phi N_{sa} = 137.22 \text{ kN}$$

$$N_{ua} = 59.52 \text{ kN} < \phi N_{sa} = 137.22 \text{ kN} ; \quad \text{OK} ; \quad \text{Ratio} = 0.43$$

3.2. Concrete Breakout Strength

Clause D.5.2

For Single Anchors:

Concrete Breakout Capacity, ϕN_{cb} :

$$\phi N_{cb} = \phi (A_{Nc}/A_{Nco}) \Psi_{ed,N} \Psi_{c,N} \Psi_{cp,N} N_b$$

where:

$$\phi = 0.7 \quad \text{Clause D.4.3}$$

$$h'_{ef} = \text{Effective embedment depth} = 80 \text{ mm}$$

$$A_{Nc} = \text{Projected concrete failure area of group of anchors} = 202500 \text{ mm}^2$$

$$A_{Nco} = \text{Projected concrete failure area of a single anchor with an edge distance equal to or greater than } 1.5 h_{ef}$$

$$= 9 h_{ef}^2 = 57600 \text{ mm}^2$$

$$\Psi_{c,N} = 1.25 \quad \text{Clause 5.2.6}$$

$$\Psi_{ed,N} = 1.00 \quad \text{Clause 5.2.5}$$

$$\Psi_{cp,N} = 1.00 \quad \text{Clause 5.2.7}$$

$$N_b = k_c \lambda a \sqrt{f'_c} h_{ef}^{1.5} \quad \text{Clause D.5.2.2}$$

$$= 40.5 \text{ kN}$$

where:

$$k_c = \text{coefficient for basic concrete breakout}$$

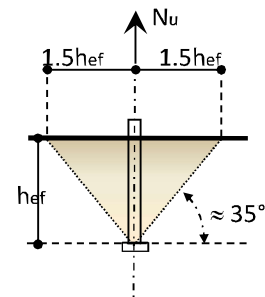
$$= 10$$

$$\lambda a = 1.00 \quad \text{Clause D.3.6}$$

$$N_{cb} = 177.88 \text{ kN}$$

$$\phi N_{cb} = 124.51 \text{ kN}$$

$$N_{ua} = 59.52 \text{ kN} < \phi N_{cb} = 124.51 \text{ kN} ; \quad \text{OK} ; \quad \text{Ratio} = 0.48$$



DESIGN OF ANCHOR SYSTEM IN CONCRETE

ACI 318M-11 APPENDIX D

Check if Anchor Group effects shall be considered: $s_{min} < 3 h_e$

For Anchor Group:

Concrete Breakout Capacity, ϕN_{cbg} :

$$\begin{aligned}\phi N_{cbg} &= \phi (A_{Nc} / A_{Nco}) \Psi_{ec,N} \Psi_{ed,N} \Psi_{c,N} \Psi_{cp,N} N_b \\ \Psi_{ec,N} &= 1 / (1 + 2 e'_N / 3 h_{ef}) \quad \text{Clause D.5.2.4} \\ &= 1.00\end{aligned}$$

where:

e'_N = distance between resultant tension on a group of anchors loaded in tension and centroid of the group of anchors loaded in tension

e'_N = mm Provide input value if applicable and zero if not applicable

$$N_{cbg} = 177.88 \text{ kN}$$

$$\phi N_{cbg} = 124.51 \text{ kN}$$

$$N_{uag} = 119.05 \text{ kN} < \phi N_{cbg} = 124.51 \text{ kN} ; \quad \text{OK} ; \quad \text{Ratio} = 0.96$$

Consider Tension Reinforcement?

Excess Tension, T_{net} :

$$\begin{aligned}T_{net} &= N_{ua} - \phi N_{cbg} \\ &= - \text{ kN}\end{aligned}$$

Diameter of Provided Steel Reinforcement

Required No. of Additional Tension Reinforcement Bars, n_{tb}

$$n_{tb} = T_{net} / (\phi A_s b f_y b)$$

where:

$$\begin{aligned}A_s b &= \text{Cross-sectional area of steel reinforcement provided} \\ &= 113.1 \text{ mm}^2 \\ f_y b &= \text{Yield Strength of Steel Reinforcement} \\ &= \text{420} \text{ Mpa} \\ \phi &= 0.9\end{aligned}$$

Therefore,

$$n_{tb} = - T - \text{ additional tension reinforcement required}$$

3.3. Pullout Strength

Clause D.5.3

Pullout Capacity, ϕN_{pn} :

$$\phi N_{pn} = \phi \Psi_{c,p} N_p$$

where:

$$\begin{aligned}\phi &= 0.7 \quad \text{Clause D.4.3} \\ \Psi_{c,p} &= 1.00 \quad \text{Clause D.5.3.6}\end{aligned}$$

For single headed stud or headed bolt: Clause D.5.3.4

$$\begin{aligned}N_p &= 8 A_{brg} f'_c \\ &= 100.53 \text{ kN}\end{aligned}$$

where:

$$\begin{aligned}d_n &= \text{diameter of Anchor Nut} = 30 \text{ mm} \\ A_{brg} &= \text{net bearing area of the head of anchor}\end{aligned}$$

DESIGN OF ANCHOR SYSTEM IN CONCRETE

ACI 318M-11 APPENDIX D

$$N_{pn} = 100.53 \text{ kN} = 392.7 \text{ mm}^2$$

$$\phi N_{pn} = 70.37 \text{ kN}$$

For single hooked bolt: Clause D.5.3.5

$$N_p = 0.9 f'_c e_h da \quad \text{where:}$$

$$e_h = \text{distance from the inner surface of the shaft of a J- or L-bolt to the outer tip of J- or L-bolt (3da} \leq e_h \leq 4.5da)$$

$$= \boxed{0} \text{ mm}^2 \quad \text{Provide input value if applicable and zero if not applicable}$$

$$N_{pn} = - \text{ kN}$$

$$\phi N_{pn} = - \text{ kN}$$

For single headed stud or headed bolt:

$$N_{ua} = 59.52 \text{ kN} < \phi N_{pn} = 70.37 \text{ kN} ; \quad \text{OK} ; \quad \text{Ratio} = 0.85$$

For single hooked bolt:

$$N_{ua} = - \text{ kN} - \phi N_{pn} = - \text{ kN} ; \quad - ; \quad \text{Ratio} = -$$

3.4. Concrete side-face blowout strength of a headed anchor Clause D.5.4

For Single Anchors:

Side-face Blowout Capacity, ϕN_{sb} :

$$\phi N_{sb} = \phi (13 C_{a1} \sqrt{A_{brg}}) \lambda a f'_c$$

where:

$$\phi = 0.7 \quad \text{Clause D.4.3}$$

$$C_{a1} = \text{distance from the center of an anchor shaft to the edge of concrete in one direction / minimum edge distance}$$

$$= 120 \text{ mm}$$

$$C_{a2} = \text{distance from the center of an anchor shaft to the edge of concrete in the direction perpendicular to } C_{a1}$$

$$= 120 \text{ mm}$$

$$A_{brg} = \text{net bearing area of the head of anchor}$$

$$= 392.7 \text{ mm}^2$$

$$\lambda a = 1.00$$

$$\text{Consider if } 1.0 \leq C_{a2}/C_{a1} \leq 3.0: \quad \text{Yes} \quad C_{a2}/C_{a1} = 1.00$$

$$N_{sb} = 174.88 \text{ kN}$$

$$\phi N_{sb} = 61.21 \text{ kN}$$

$$N_{ua} = 59.52 \text{ kN} < \phi N_{sb} = 61.21 \text{ kN} ; \quad \text{OK} ; \quad \text{Ratio} = 0.97$$

Check if Anchor Group effects shall be considered: $s_{min} < 2 c_{Na}$

For Anchor Group:

Side-face Blowout Capacity, ϕN_{sbg} :

$$\phi N_{sbg} = \phi (1 + (s/6 C_{a1})) N_{sb}$$

DESIGN OF ANCHOR SYSTEM IN CONCRETE

ACI 318M-11 APPENDIX D

$$N_{sb} = 174.88 \text{ kN}$$

$$\phi N_{sbg} = 122.41 \text{ kN}$$

$$N_{uag} = 119.05 \text{ kN} < \phi N_{sbg} = 122.41 \text{ kN} ; \quad \text{OK} ; \quad \text{Ratio} = 0.97$$

3.5. Bond Strength of Adhesive Anchor Clause D.5.5

For Single Anchors:

Bond Strength Capacity, ϕN_a :

$$\phi N_a = \phi (A_{Na}/A_{Na0}) \Psi_{ed,Na} \Psi_{cp,Na} N_{ba}$$

where:

$$\phi = 0.7$$

A_{Na} = projected influence area of group of adhesive anchors

$$= 202500 \text{ mm}^2$$

A_{Na0} = Projected influence area of a single anchor if not limited by edge distance or spacing

$$= (2c_{Na})^2 \text{ (If } c_{Na} > \text{edge distance)}$$

$$= 57600 \text{ mm}^2$$

$$c_{Na} = 10 d_a \sqrt{(\tau_{uncr}/7.6)}$$

$$= 154 \text{ mm}$$

$$\tau_{uncr} = 4.5 \text{ Table D.5.5.2}$$

Service Environment:

Outdoor ▼

$$\Psi_{ed,Na} = 0.93 \text{ Clause D.5.5.4}$$

$$\Psi_{cp,Na} = 1.00 \text{ Clause D.5.5.5}$$

$$N_{ba} = \lambda_a \tau_{cr} \pi d_a D$$

$$= 35.19 \text{ kN}$$

where:

$$\lambda_a = 1.00 \text{ Clause D.3.6}$$

$$\tau_{cr} = 1.4 \text{ Table D.5.5.2}$$

$$N_a = 115.53 \text{ kN}$$

$$\phi N_a = 86.64 \text{ kN}$$

$$N_{ua} = 59.524 \text{ kN} < \phi N_{ag} = 86.64 \text{ kN} ; \quad \text{OK} ; \quad \text{Ratio} = 0.69$$

Check if Anchor Group effects shall be considered: $s_{min} < 2 c_{Na}$

Check:

For Anchor Group:

Bond Strength Capacity, ϕN_{ag} :

$$\phi N_{ag} = \phi (A_{Na}/A_{Na0}) \Psi_{ec,Na} \Psi_{ed,Na} \Psi_{cp,Na} N_{ba}$$

$$\Psi_{ec,Na} = 1 / (1 + e'_N / c_{Na}) \text{ Clause D.5.5.3}$$

$$= 1.00$$

where:

e'_N = distance between resultant tension on a group of anchors loaded in tension and centroid of the group of anchors loaded in tension

$$N_{ag} = 115.53 \text{ kN}$$

$$\phi N_{ag} = 80.87 \text{ kN}$$

$$e'_N = \boxed{0} \text{ mm} \text{ Provide input value if applicable and zero if not applicable}$$

$$N_{uag} = 119.05 \text{ kN} > \phi N_{ag} = 80.87 \text{ kN} ; \text{ NOT OK} ; \text{ Ratio} = 1.47$$

4. Verification of Anchors against Shear

For Single Anchor:

Check Applied Shear for each Anchor, V_{ua}

$$\begin{aligned} V_{ua} &= \sqrt{(V_x^2 + V_y^2)} / N \\ &= 1.00 \text{ kN} \end{aligned}$$

For Anchor Group:

Check Applied Shear for group of anchors, V_{uag}

$$\begin{aligned} V_{uag} &= \sqrt{(V_x^2 + V_y^2)} \\ &= 4.00 \text{ kN} \end{aligned}$$

4.1. Steel Strength of Anchor Clause D.6.1

Shear Capacity of each Anchor, ϕV_{sa} :

$$\phi V_{sa} = 0.6 A_{se,V} f_{uta}$$

where:

$$\phi = 0.7 \quad \text{Clause D.4.3}$$

$$A_{se,V} = \text{Effective Cross-Sectional Area of Anchor} = 245.04 \text{ mm}^2$$

$$f_{uta} = \text{Nominal Tensile Strength of Anchors} = 800 \text{ MPa}$$

$$V_{sa} = 117.62 \text{ kN}$$

$$\phi V_{sa} = 82.33 \text{ kN}$$

$$V_{ua} = 1.00 \text{ kN} < \phi V_{sa} = 82.33 \text{ kN} ; \text{ OK} ; \text{ Ratio} = 0.01$$

4.2. Concrete Shear Breakout Strength Clause D.6.2

For Single Anchors:

Concrete Breakout Capacity, ϕV_{cbg} :

$$\phi V_{cb} = \phi (A_{Vc} / A_{Vco}) \Psi_{ed,V} \Psi_{c,V} \Psi_{h,V} V_b$$

where:

$$\phi = 0.7$$

$$c'_{a1} = \text{Effective embedment depth} = 120 \text{ mm}$$

$$\begin{aligned} A_{Vc} &= \text{Projected concrete failure area of groups of anchor} \\ &= 54000 \text{ mm}^2 \end{aligned}$$

$$\begin{aligned} A_{Vco} &= \text{Projected concrete failure area for a single anchor} \\ &= 4.5(c'_{a1})^2 \\ &= 64800 \text{ mm}^2 \end{aligned}$$

$$\begin{aligned} h_a &= \text{thickness of member in which an anchor is located, measured parallel to anchor axis.} \\ &= 350 \text{ mm} \end{aligned}$$

$$\begin{aligned} \Psi_{c,V} &= \text{modification factor based on presence or absence of cracks in concrete} \\ &= 1.00 \end{aligned}$$

DESIGN OF ANCHOR SYSTEM IN CONCRETE

ACI 318M-11 APPENDIX D

$$\Psi_{ed,V} = 0.70 \quad \text{Clause D.6.2.6}$$

$$\Psi_{h,V} = 1.00 \quad \text{Clause D.6.2.8}$$

$$\begin{aligned} V_b &= (0.6 (\ell_e/d_a)^{0.2} V_{d_a}) \lambda_a v_f' c (C_{a1})^{1.5} & \text{where:} \\ &= 30.24 \text{ kN} & \ell_e &= 160 \text{ mm} \\ V_b &= 3.7 \lambda v_f' c (C_{a1})^{1.5} & \lambda_a &= 1.00 \quad \text{Clause D.3.6} \\ &= 27.514 \text{ kN} \end{aligned}$$

$$\phi V_{cb} = 16.05 \text{ kN}$$

$$\phi V_{cb} = 11.23 \text{ kN}$$

$$V_{ua} = 1.00 \text{ kN} < \phi V_{cb} = 11.23 \text{ kN} ; \quad \text{OK} ; \quad \text{Ratio} = 0.09$$

For Anchor Group:

Concrete Breakout Capacity, ϕV_{cbg} :

$$\phi V_{cbg} = \phi (A_{Vc}/A_{Vco}) \Psi_{ec,V} \Psi_{ed,V} \Psi_{c,V} \Psi_{h,V} V_b$$

$$\begin{aligned} \Psi_{ec,V} &= 1 / (1 + 2 e'_V / 3 c_{a1}) & \text{Clause D.6.2.5} \\ &= 1.00 \end{aligned}$$

where:

e'_V = distance between resultant shear on a group of anchors loaded in shear in the same direction, and the centroid of the group of anchors in same direction

$$e'_V = \boxed{0} \text{ mm} \quad \text{Provide input value if applicable and zero if not applicable}$$

$$\phi V_{cb} = 16.05 \text{ kN}$$

$$\phi V_{cb} = 11.23 \text{ kN}$$

$$V_{uag} = 4.00 \text{ kN} < \phi V_{cbg} = 11.23 \text{ kN} ; \quad \text{OK} ; \quad \text{Ratio} = 0.36$$

4.3. Pryout Strength Clause D.6.3

For Single Anchors:

Pryout Capacity, ϕV_{cp} :

$$\phi V_{cp} = \phi k_{cp} N_{cp}$$

where:

$$N_{cp} = 177.9 \text{ kN}$$

$$k_{cp} = 2.00$$

$$\phi = 0.7$$

$$V_{co} = 355.8 \text{ kN}$$

$$\phi V_{cp} = 249.0 \text{ kN}$$

$$V_{ua} = 1.00 \text{ kN} < \phi V_{cp} = 249.03 \text{ kN} ; \quad \text{OK} ; \quad \text{Ratio} = 0.00$$

For Anchor Group:

Pryout Capacity, ϕV_{cpg} :

DESIGN OF ANCHOR SYSTEM IN CONCRETE

ACI 318M-11 APPENDIX D

$$\phi V_{cpg} = \phi k_{cp} N_{cpg}$$

where:

$$N_{cpg} = 177.9 \text{ kN}$$

$$k_{cp} = 2.00$$

$$\phi = 0.7$$

$$V_{cpg} = 355.8 \text{ kN}$$

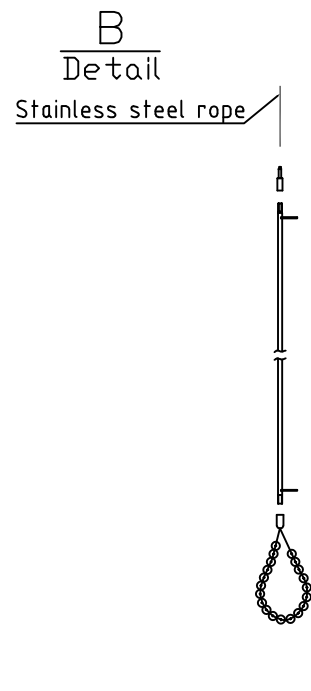
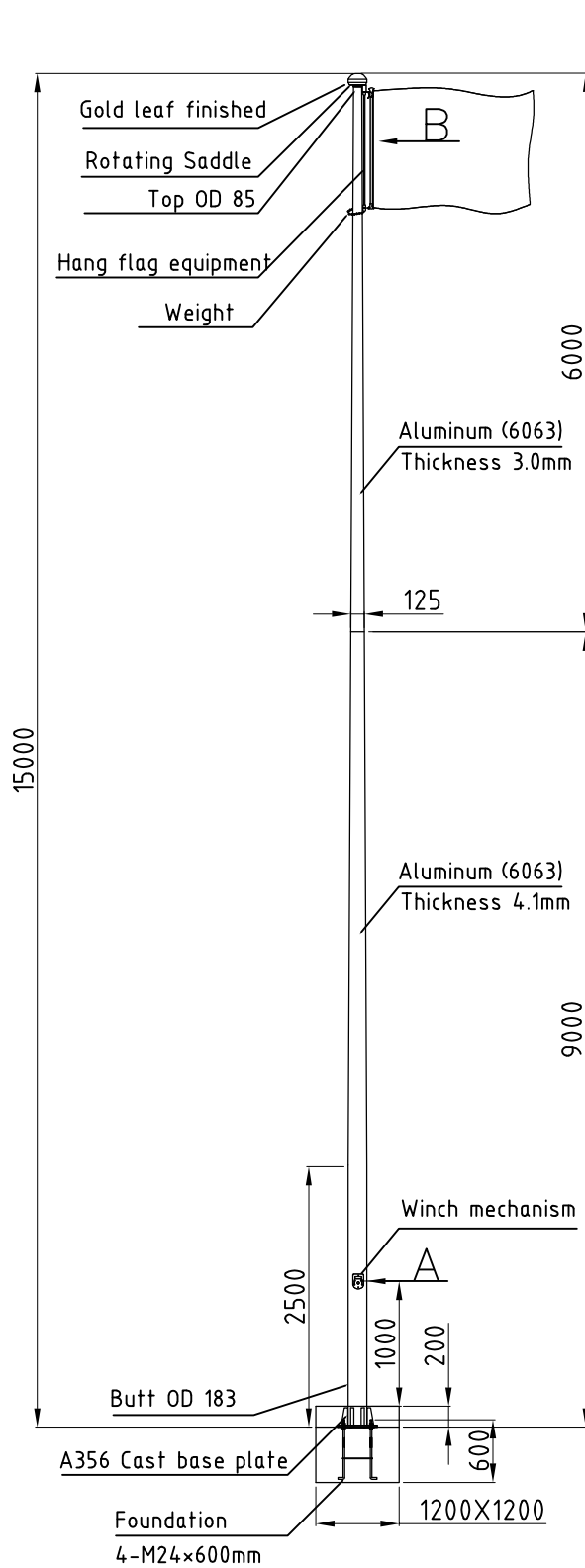
$$\phi V_{cpg} = 249.0 \text{ kN}$$

$$= 4.00 \text{ kN} < \phi V_{cpg} = 249.0 \text{ kN} ; \text{ OK} ; \text{ Ratio} = 0.02$$

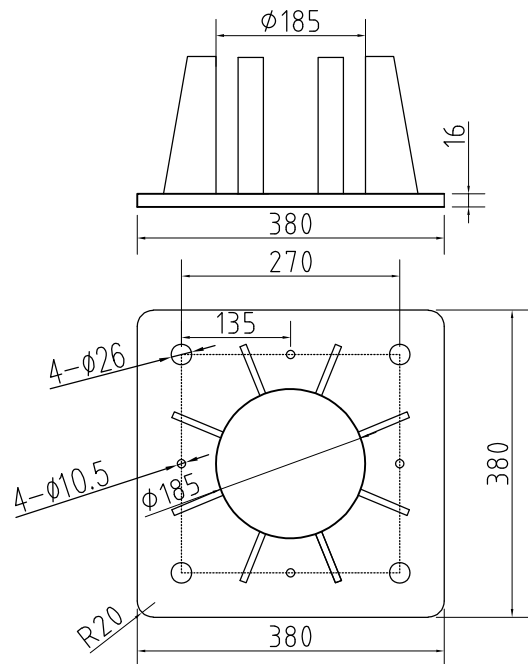
SUMMARY:

Type of Anchor	: Cast-In Anchors
Number and Diameter of Anchor	: 4 - M 24
Grade of Anchor	: Grade 8.8
Anchor Embedment Depth	: 600 mm
Area of Concrete Pedestal or Affected Concrete	: 450 x 450 mm
Compressive Strength of Concrete	: 32 MPa
Yield Strength of Steel	: 420 MPa
Tension Reinforcement in Concrete	: - T -

Summary	Ratio		Remarks
	Single	Group	
<i>Tensile Loading</i>			
Steel Strength	0.43	N/A	✓
Concrete Breakout	0.48	0.96	✓
Pullout	0.85	N/A	✓
Side-face Blowout	0.97	0.97	✓
Bond Strength	N/A	N/A	✓
<i>Shear Loading</i>			
Steel Strength	0.01	N/A	✓
Concrete Breakout	0.09	0.36	✓
Pryout	0.00	0.02	✓



Base Plate



Remark:

- 1.All dimensions are in millimeters unless otherwise stated.
- 2.Material is aluminium alloy 6063-T6.
- 3.Surface treatment is powder coating.

Itemref	Quantity	Title/Name, designation, material, dimension etc			Article No./Reference	
Designed by		Checked by	Approved by - date	Filename	Date 6 June, 2024	Scale
 PROSPEC SPECIALTIES				15m High Aluminum Flagpole		
				FPA15i Modified (Internal Halyard)		Edition